

# ANNUAL REPORT 2008

UIUC, August 6, 2008

## New features of CON1D: Version 9.6

Xiaoxu Zhou (MS Student) &  
Brian G. Thomas



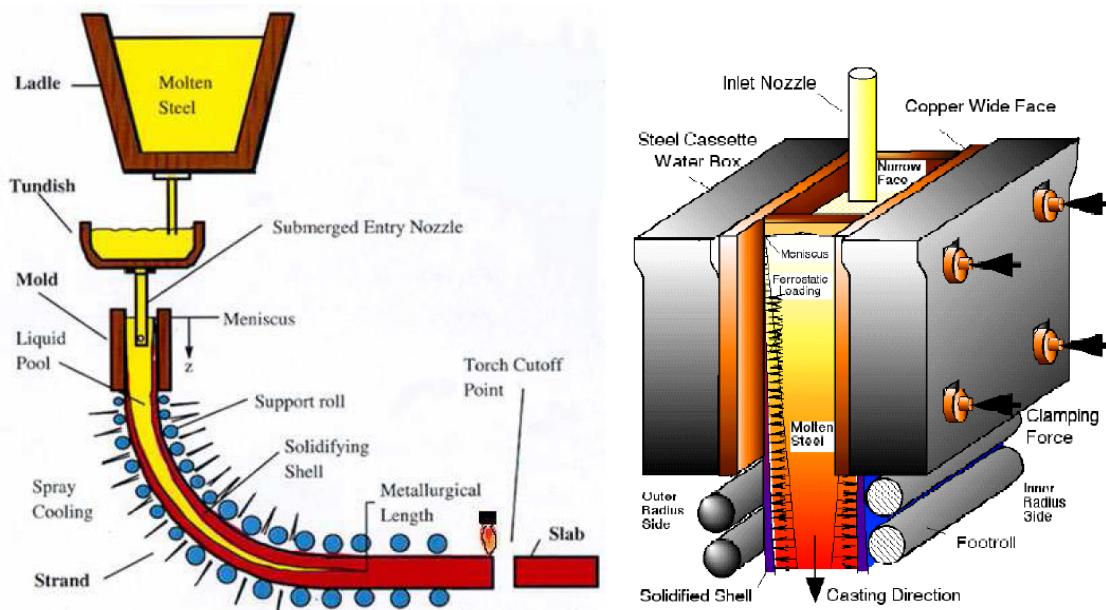
*Department of Mechanical Science and Engineering*  
University of Illinois at Urbana-Champaign



## Acknowledgements

- Continuous Casting Consortium Members
  - Baosteel, Corus, Goodrich, Labein, LWB Refractories, Mittal, Nucor, Postech, Steel Dynamics, Ansys Inc.
- National Science Foundation
  - GOALI DMI 05-00453 (Online)
- Previous students developers of Con1d:
  - Bryant Ho, Guowei Li, Nick Youssef, Ya Meng, Ying Shang, David Stone
- Previous modeling work: Huan Li, A. Behera

# Continuous casting of steel



-ccc.mechse.uiuc.edu

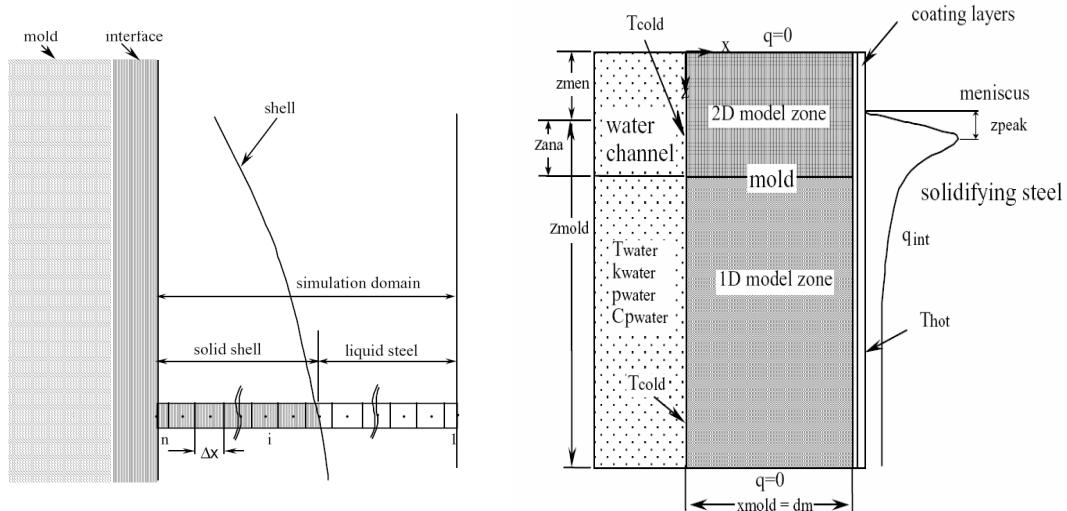
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## Review: Con1d simulation domain in the steel and mold



-Con1d9.6 user's manual

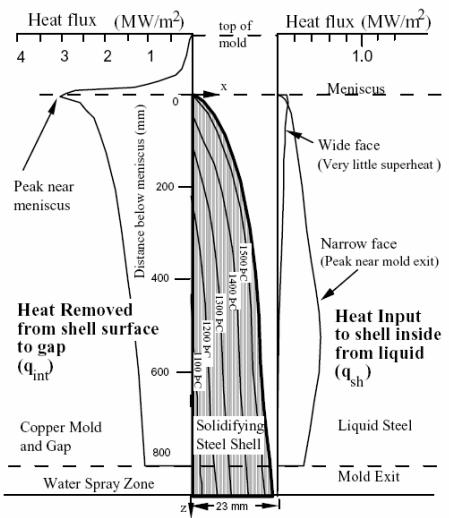
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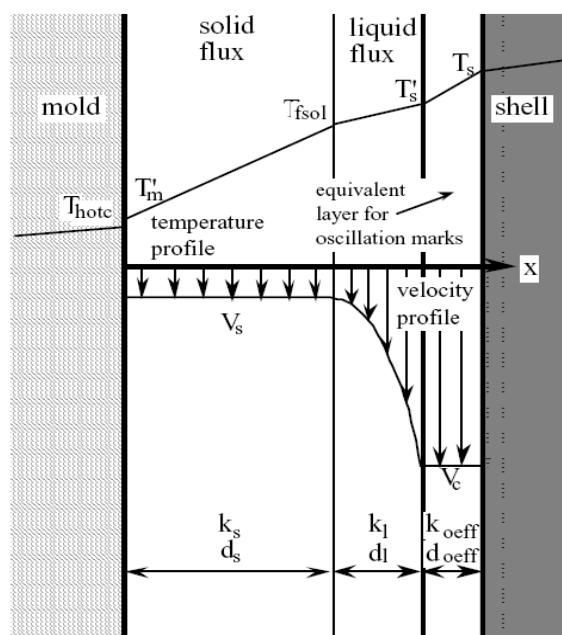
# Review: Con1d heat flux in the mold



Model of solidifying steel shell showing typical isotherms and heat flux conditions

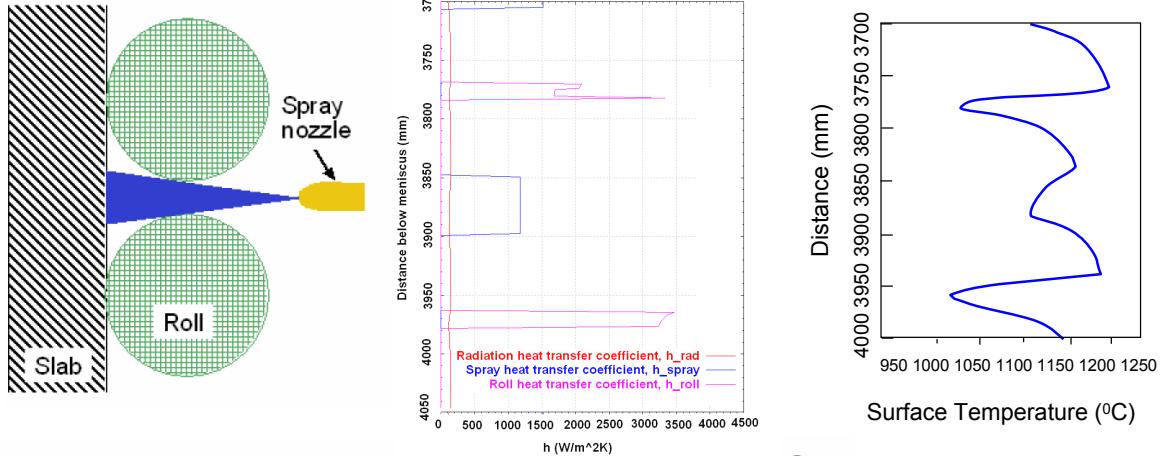
-Con1d9.6 user's manual

# Review: Velocity and temperature profile assumed across interfacial gap



-Con1d9.6 user's manual

# Review: Con1d heat transfer between rolls



$$h_{spray} = A \cdot Q_{water}^c \cdot (1 - b \cdot T_{spray}) \text{ ---Nozaki's model}$$

$$h_{rad\_spray} = \sigma \cdot \varepsilon_{steel} (T_{sK} + T_{ambK}) (T_{sK}^2 + T_{ambK}^2)$$

$$h_{roll} = \frac{f_{roll}}{L_{roll\ contact}} \cdot (1 - f_{roll}) \left( \frac{(h_{rad\_spray} + h_{conv} + h_{spray}) \cdot L_{spray} +}{(h_{rad\_spray} + h_{conv}) \cdot (L_{spray\ pitch} - L_{spray} - L_{roll\ contact})} \right)$$

$Q_{water}$  Water flux rate

$T_{spray}$  Spraying water temperature

$f_{roll}$  Fraction of heat extraction to roll

-A.Behera,2006,ccc report

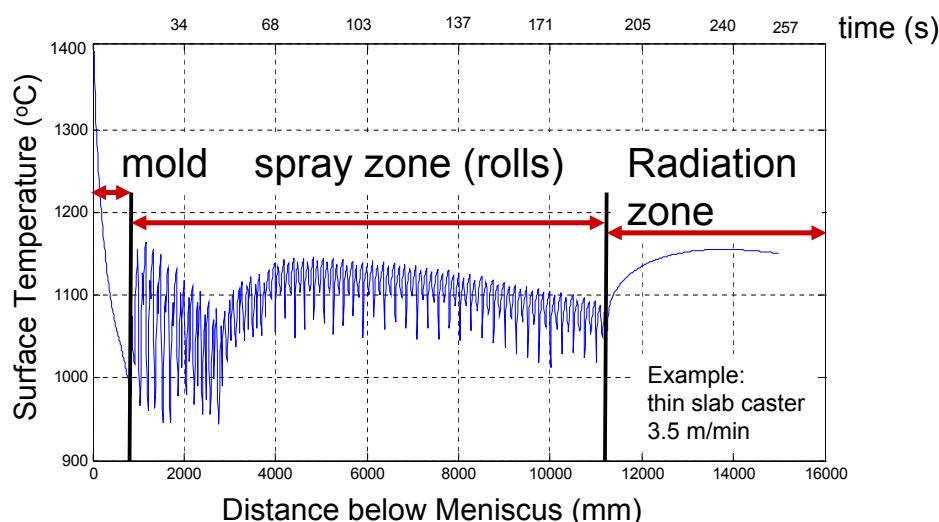
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## Con1d predicts surface temperature down strand



Note: reheating below mold; and after sprays  
variations caused by rolls (slab caster)

-A.Behera,2006,ccc report

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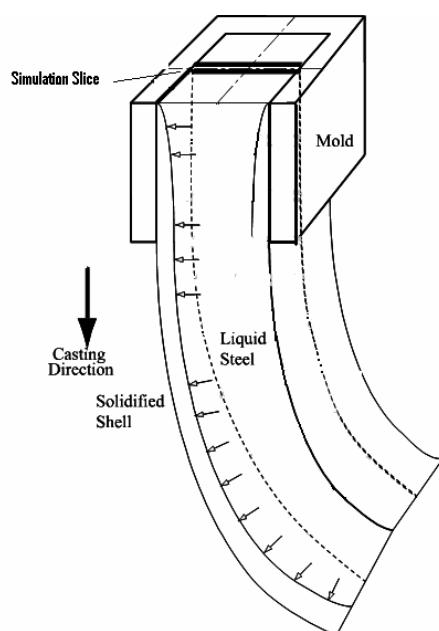
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# New features for Con1d9.6

- Several minor bugs in Con1d8.0 are fixed in Con1d9.6.
- Two new options for defining interface (mold/shell) heat flux
  - enter average mold heat flux
  - enter mold cooling water temperature increase
- New simulation domain. ([New domain](#))
- Spray zones heat transfer is assumed the same on both sides as the CON1D8 file. Changes should be made by the user to introduce differences in the CON1D9.6.
- New heat transfer coefficient profile. ([Click here](#))
- Leidenfrost effect implemented. ([Click here](#))
- Browsing the new example input file. ([Click here](#))

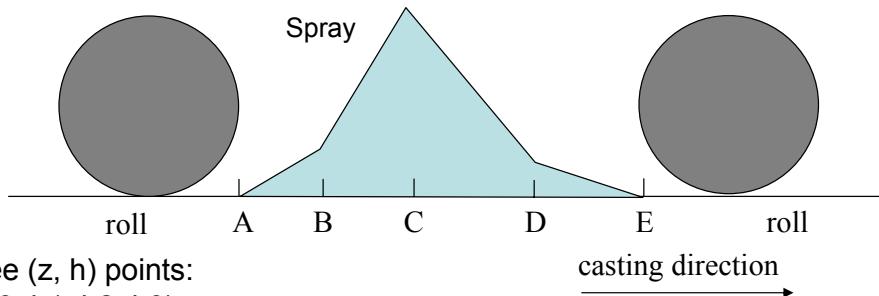
## Simulation domain for Con1d9.6



Model both sides of caster at the same time (Inside and Outside Radius)

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## Spray-nozzle heat transfer coefficient can vary along caster (input as 4 piecewise linear line segments)



Input three ( $z$ ,  $h$ ) points:

$$(z_1, z_2, z_3, h_1, h_2, h_3)$$

$$z_1=AB/AE, z_2=AC/AE, z_3=AD/AE$$

The symmetry of profile is not required.

Nozaki correlation:

$$h_{\text{spray}} = A \cdot C \cdot \bar{W}^n \cdot (1 - bT)$$

$$\cdot A \cdot C = 0.3925, b = 0.0075, n = 0.55$$

$\cdot T$  is the cooling-water spray temperature

$\cdot W$  ( $\text{L/m}^2\text{s}$ ) is the average water flow rate in the spray zones.

$\cdot h_{\text{spray}}$  gives average heat transfer coefficient in the spray zone.

$$h_A = 0$$

$$h_B = h_1 * h_{\text{spray}}$$

$$h_C = h_2 * h_{\text{spray}}$$

$$h_D = h_3 * h_{\text{spray}}$$

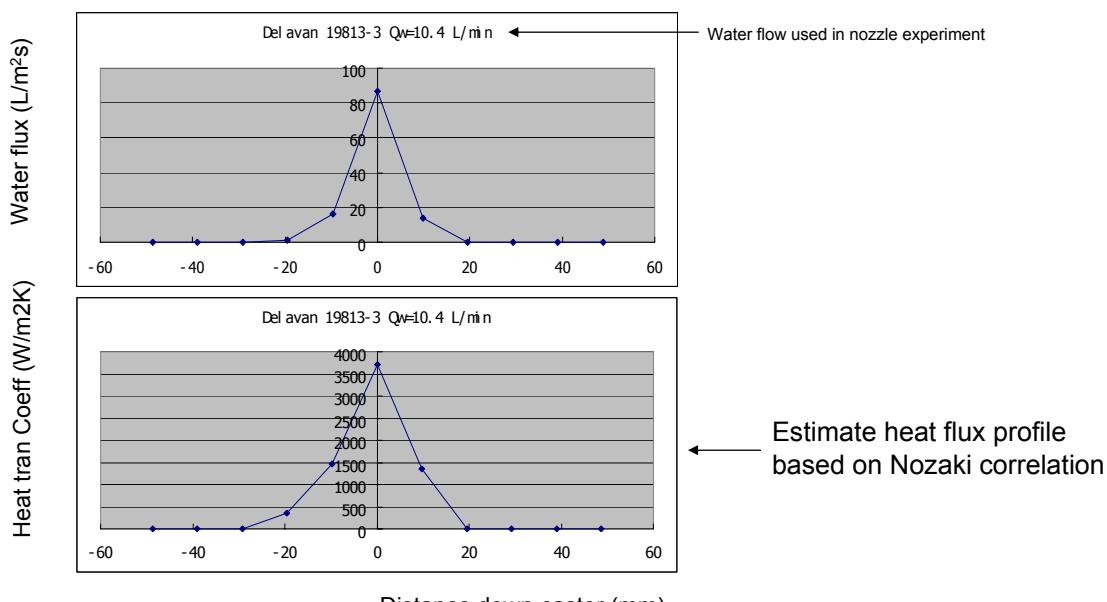
$$h_E = 0$$

Con1d8 just use  $h_{\text{spray}}$  in the spray zone.

## Example $h$ profile

--from Vapalahti's 2006 ccc meeting report:

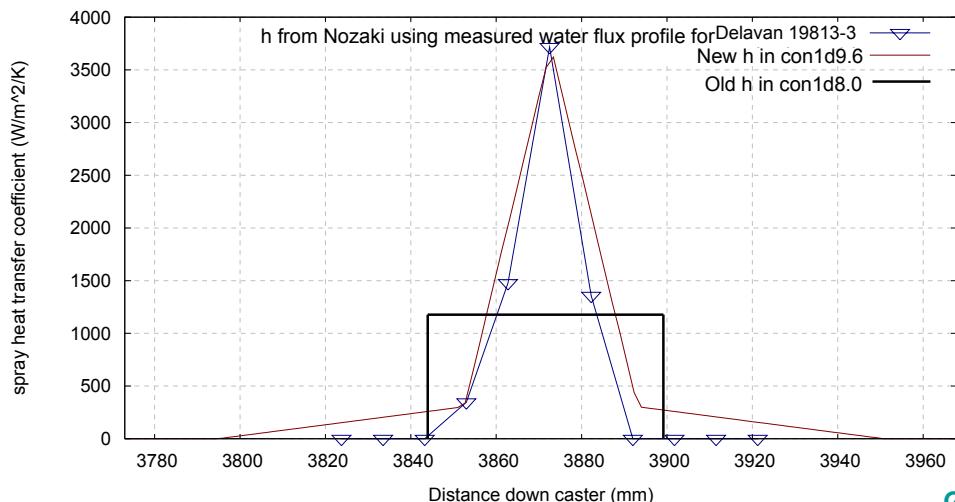
"Delavan Nozzle Characterization at CINVESTAV"



# Compare h profiles

- New h profile in Con1d 9.6:
  - $z_1 \ z_2 \ z_3 \ h_1 \ h_2 \ h_3$
  - 0.37 0.50 0.63 0.50 6.11 0.50

• The spray length is properly elongated due to the accumulation of water on the strand.



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Delavan 19813-3 campaign

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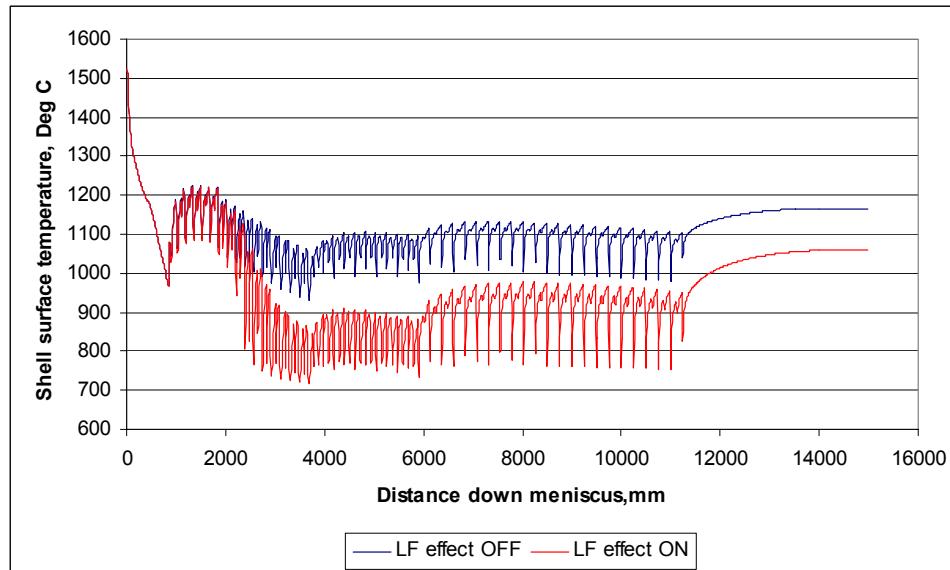
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# Leidenfrost effect (optional)

- To increase  $h$  to account for boiling heat transfer effect, a set of multipliers can be input to Con1d, such as follows:

<b>h-multipliers</b>	1.0	1.2	2.2	1.6	1.0
<b>temperatures</b>	700.	800	900.	1000	1050.

# Leidenfrost effect on shell surface temperature prediction



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# Con1d9.6 input file

CON1D-9.6 Slab Casting Heat Transfer Analysis  
University of Illinois, Brian G. Thomas, 2008

Example Input Data (NU6-146)

```
#1 Parameters to update every call
//CASTING CONDITION:
 3      Number of time-cast speed data points
        (If=1, constant casting speed)
        Next 2 lines contain time(s) and vc(m/min) data points
 0.300.320.
3.70 3.70 4.70
1553.000 Pour temperature (C)
100.0000 Distance of meniscus from top of mold (mm)
150.0000 Nozzle submergence depth (mm)

 0      New simulation or Restart (0=new; 1=restart)
15000.00 Max. simulation length (must > z-distance)(mm)

 0      Calculate mold and interface (=0 flux casting, or =2 oil casting )
        or enter interface heat flux data starting at meniscus z=0 (=1)
        or enter avg. mold flux (=2), or enter cooling water temp. increase (=3)
 9      Number of zmm and q data points (if above = -1)
        Next 2 lines contain zmm(mm) and q(kW/m2) data
 0.00 40.00 100.00 200.00 300.00 410.00 550.00 850.00 950.00
5360.00 4000.00 3410.00 2600.00 2350.00 2340.00 2310.00 2000.00 2000.00
2.4243 2.4243 Average mold heat flux (MW/m2)(if above =-2)
-9.8800 -9.8800 Mold cooling water temp. increase (Deg C)(if above =-3)
-1      Running mode (0=stop right now; -1=continue to run; positive integer ts
        = run the program for ts seconds.
```

# Con1d9.6 input file (Cont...)

//SPRAY ZONE VARIABLES:

8.700000 Minimum convection heat trans. coeff. (natural) (W/m^2K)  
 right side (inside radius):  
 25.00000 Water and ambient temperature after spray zone(Deg C)  
 spray zone condition:(heat tran.coeff.funct:h=A\*C\*W^n(1-bT))  
 (Nozaki Model:A\*C=0.3925,n=0.55,b=0.0075)  
 1.570000 A(0=off)  
 0.5500000 n  
 7.499998E-03 b

11 Number of zones

No.	zone	rol.	water starts	spray # rad.	flowrate	width	length	angle	frac.of q thr	spray rol	conv coeff	amb. temp.	(W/m^2K)	(C)	z1	z2	z3	h1	h2	h3
1	850.0	1	0.062	89.900	1.640	0.050	10.00	0.010	0.250	8.70	25.0	0.08	0.50	0.92	0.30	1.22	0.30			
2	940.0	5	0.062	172.300	0.987	0.050	10.00	0.080	0.250	8.70	25.0	0.19	0.50	0.81	0.50	0.97	0.50			
3	1767.0	6	0.062	107.800	0.987	0.050	10.00	0.220	0.250	8.70	25.0	0.14	0.50	0.86	0.70	1.36	0.70			
4	2828.3	5	0.070	31.200	1.008	0.170	10.00	0.200	0.250	8.70	25.0	0.30	0.50	0.70	0.30	5.36	0.30			
5	3773.6	1	0.080	11.000	1.620	0.176	10.00	0.360	0.250	8.70	25.0	0.37	0.50	0.63	0.50	6.11	0.50			
6	3968.6	9	0.080	11.000	1.620	0.176	10.00	0.360	0.250	8.70	25.0	0.37	0.50	0.63	0.50	6.11	0.50			
7	5903.6	1	0.095	15.200	1.680	0.204	10.00	0.360	0.250	8.70	25.0	0.34	0.50	0.66	0.02	0.92	0.02			
8	6130.3	9	0.095	15.200	1.680	0.204	10.00	0.360	0.250	8.70	25.0	0.34	0.50	0.66	0.02	0.92	0.02			
9	8260.0	1	0.095	19.700	1.680	0.212	10.00	0.360	0.250	8.70	25.0	0.39	0.50	0.61	0.01	1.13	0.01			
10	8495.8	10	0.095	19.700	1.680	0.212	10.00	0.360	0.250	8.70	25.0	0.39	0.50	0.61	0.01	1.13	0.01			
11	10995.8	1	0.115	19.700	1.680	0.212	10.00	0.360	0.250	8.70	25.0	0.39	0.50	0.61	0.01	1.13	0.01			

11246.0 End of last spray zone (mm)

0 Consider Leidenfrost effect? (-1=yes;0=no)

5 Number of points in the Leidenfrost effect curve (if above =-1)

Next 2 lines contain Leidenfrost effect h-multipliers and temperatures

1.0 3.5 2.8 1.3 1

700. 800. 900. 1000. 1100.

# Con1d9.6 input file (Cont...)

left side (outside radius):

25.00000 Water and ambient temperature after spray zone(Deg C)  
 spray zone condition:(heat tran.coeff.funct:h=A\*C\*W^n(1-bT))  
 (Nozaki Model:A\*C=0.3925,n=0.55,b=0.0075)  
 1.570000 A(0=off)  
 0.5500000 n  
 7.499998E-03 b

11 Number of zones

No.	zone	rol.	water starts	spray # rad.	flowrate	width	length	angle	frac.of q thr	spray rol	conv coeff	amb. temp.	(W/m^2K)	(C)	z1	z2	z3	h1	h2	h3
1	850.0	1	0.062	89.900	1.640	0.050	10.00	0.010	0.250	8.70	25.0	0.08	0.50	0.92	0.30	1.22	0.30			
2	940.0	5	0.062	172.300	0.987	0.050	10.00	0.080	0.250	8.70	25.0	0.19	0.50	0.81	0.50	0.97	0.50			
3	1767.0	6	0.062	107.800	0.987	0.050	10.00	0.220	0.250	8.70	25.0	0.14	0.50	0.86	0.70	1.36	0.70			
4	2828.3	5	0.070	31.200	1.008	0.170	10.00	0.200	0.250	8.70	25.0	0.30	0.50	0.70	0.30	5.36	0.30			
5	3773.6	1	0.080	11.000	1.620	0.176	10.00	0.360	0.250	8.70	25.0	0.37	0.50	0.63	0.50	6.11	0.50			
6	3968.6	9	0.080	11.000	1.620	0.176	10.00	0.360	0.250	8.70	25.0	0.37	0.50	0.63	0.50	6.11	0.50			
7	5903.6	1	0.095	15.200	1.680	0.204	10.00	0.360	0.250	8.70	25.0	0.34	0.50	0.66	0.02	0.92	0.02			
8	6130.3	9	0.095	15.200	1.680	0.204	10.00	0.360	0.250	8.70	25.0	0.34	0.50	0.66	0.02	0.92	0.02			
9	8260.0	1	0.095	19.700	1.680	0.212	10.00	0.360	0.250	8.70	25.0	0.39	0.50	0.61	0.01	1.13	0.01			
10	8495.8	10	0.095	19.700	1.680	0.212	10.00	0.360	0.250	8.70	25.0	0.39	0.50	0.61	0.01	1.13	0.01			
11	10995.8	1	0.115	19.700	1.680	0.212	10.00	0.360	0.250	8.70	25.0	0.39	0.50	0.61	0.01	1.13	0.01			

11246.0 End of last spray zone (mm)

0 Consider Leidenfrost effect? (-1=yes;0=no)

5 Number of points in the Leidenfrost effect curve (if above =-1)

Next 2 lines contain Leidenfrost effect h-multipliers and temperatures

1.0 3.5 2.8 1.3 1

700. 800. 900. 1000. 1100.

# Con1d9.6 input file (Cont...)

---

```
//MOLD COOLING WATER PARAMETERS:
43.00000 Cooling water temperature at mold top(C)
0.6200000 Cooling water pressure(MPa)
1 Form of cooling water velocity/flowrate(1=m/s ; 2=L/s)
-8.500000 -8.500000 Cooling water velocity/flowrate per face (WF,NF)
          (> 0 cooling water from mold top to bottom
           < 0 cooling water from mold bottom to top)

#2 Parameters to update every heat:
//SLAB GEOMETRY:
90.00000 Slab thickness (mm)
1396.000 Slab width (mm)
950.0000 Total mold length (mm)
35.00000 WF Mold thickness with water channel (mm),(outer rad.,top)
35.00000 WF Mold thickness with water channel (mm),(inner rad.,top)

//STEEL PROPERTIES:
0.0600 1.1500 0.0020 0.0100 0.1880 %C,%Mn,%S,%P,%Si
0.0400 0.0400 0.1200 0.0100 0.0020 %Cr,%Ni,%Cu,%Mo,%Ti
0.0200 0.0010 0.0080 0.0350 0.0000 %Al,%V,%N,%Nb,%W
0.0000 %Co,(additional components)
1000 Grade flag
(1000,304,316,317,347,410,419,420,430,999)
1 If CK simple Seg. Model wanted for default Tliq,Tsol
(1=yes,0=no)
10.00000 Cooling rate used in Seg.Model(if above =1) (K/sec)
Override defaults with following constants(-1=default)
-1.000000 Steel liquidus temperature (C)
-1.000000 Steel solidus temperature (C)
-1.000000 Steel density (g/cm^3)
-1.000000 Heat fusion of steel (kJ/kg)
-1.000000 Steel emissivity (-)
-1.000000 Steel specific heat (kJ/kg deg K)
-1.000000 Steel thermal conductivity (W/mK)
-1.000000 Steel thermal expansion coeff. (/K)
```

# Con1d9.6 input file (Cont...)

---

```
#3 Parameters to update when model is calibrated
//SIMULATION PARAMETERS:
849.0000 Z-distance for heat balance (mm)
0 Which shell to consider? (0=narrow face; 1=wide face)
0 What type of mold?(0=slab, 1=funnel, 2=billet, -1=shell only)
2 Which moldface to consider? (1=curved, 2=straight)
1.000000 Is superheat treated as heatflux?
0=no; 1=yes (take default); -1=yes (enter data)
17 Number of zmm and q data points(if above =-1)
Next 2 lines contain zmm(mm) and q(kW/m2) data
10. 45. 100. 200. 300. 400. 500. 675. 720. 770. 980. 1120. 1370. 1470. 1575. 1700. 2000.
20. 40. 58. 57. 28. 36. 88. 384. 408. 406. 321. 303. 98. 58. 38. 25. 20.
1 Do you want (more accurate) 2d calculations in mold?
(0=no; 1=yes; 2=yes, one extra loop for better taper)
850.0000 Max. dist. below meniscus for 2d mold cales (mm)
(=mold length if above = 2)
3.000000E-03 Time increment (s)
180 Number of slab sections
10.00000 Printout interval (mm)
0.000000E+00 Start output at (mm)
90.00000 Max. simulation thickness (mm)
(Usually the slab thickness)
200000 Max. number of iterations
3 Shell thermocouple numbers below hot face (less than 10)
Next line gives the distance below surface of thermocouples(mm)
10.0 12.5 25.0
0.700000 Fraction solid for shell thicknesss location (-)
0 Do you want to print all the files for the related information for each slice?
(0=no; 1=yes); (remark: choosing 1 would slow down the program)
```

# Con1d9.6 input file (Cont...)

---

```
//MOLD FLUX PROPERTIES:
38.36 38.08 0.73 13.47 0.46 %CaO,%SiO2,%MgO,%Na2O,%K2O
0.00 0.89 0.00 0.00 %FeO,%Fe2O3,%NiO,%MnO,%Cr2O3
3.27 0.01 0.00 0.01 0.00 %Al2O3,%TiO2,%B2O3,%Li2O,%SrO
0.00 8.60 0.33 0.00 0.23 %ZrO2,%F,%free C,%total C,%CO2
1      number of Tfso1 and viscosity exponent n
Next 3 lines contain zmm(mm) and tfol and expn data
0.
1183.00
2.700
1.000000 Solid flux conductivity(W/mK)
1      number of Liquid flux conductivity data
Next 2 lines contain zmm and Tkliquid data
0.
1.500
0.9000000 Flux viscosity at 1300C (poise)
2600.000 Mold flux density(kg/m^3)
250.0000 Flux absorption coefficient(1/m)
-1.000000 Flux index of refraction(-)
(-1 = take default f(composition))
0.9000000 Slag emissivity(-)
1      Form of mold powder consumption rate(1=kg/m^2; 2=kg/t)
5.5700000E-02 Mold powder consumption rate
3.5000000E-02 Location of peak heat flux (m)
1.000000 Slag rim thickness at metal level (meniscus) (mm)
7.0000000E-02 Slag rim thickness at heat flux peak (mm)
3.500000 Liquid pool depth (mm)
80.00000 Solid flux tensile fracture strength (KPa)
8000.000 Solid flux compress fracture strength (KPa)
0.1700000 Solid flux Poisson ratio(-)
1      number of slag static friction coeff data
Next 2 lines contain zmm and Static friction coeff
0.
0.500
0.5000000 Moving friction coefficient between solid flux and mold wall
```

# Con1d9.6 input file (Cont...)

---

```
//INTERFACE HEAT TRANSFER VARIABLES:
2      Number of distance-ratio data points
(1=constant ratio of solid flux velocity
to casting speed)
Next 2 lines contain zmm(mm) and ratio(-) data
0.1000.
0.000 0.128
9.500003E-05 Flux/mold or shell/mold contact resistance(m^2K/W)
0.5000000 Mold surface emissivity(-)
5.999999E-02 Air conductivity(in oscillation marks)(W/mK)
0      Osc.marks simulation flag(0=average,1=transient)
7.999999E-02 Oscillation mark depth(mm)
1.500000 Width of oscillation mark (mm)
3.750000 Oscillation frequency(cps)
(-1=take default cpm=2*ipm casting speed)
6.200000 Oscillation stroke(mm)

//MOLD WATER PROPERTIES:
-1.000000 heat transfer coefficient(W/m^2K)
(-1=defaul=f(T), based on Slezach and Rouse Eqn)
-1.000000 Water heat capacity(J/kgK)(-1=defaul=f(T))
-1.000000 Water density(kg/m^3)(-1=defaul=f(T))

//MOLD GEOMETRY:
41.00000 Narrow face (NF) mold thickness with water channel (mm)
56.00000 Equivalent thickness of water box (mm)
-1.000000 Mean temperature diff between hot & cold face of NF (C)
14.00000 17.00000 Cooling water channel depth(mm)(WF,NF)
5.000000 9.000000 Cooling water channel width(mm)(WF,NF)
13.00000 21.00000 Channel distance(center to center)(mm)(WF,NF)
-1.000000 -1.000000 Total channel cross sectional area(mm^2)(WF,NF)
(served by water flow line where temp rise measured)
350.0000 350.0000 Mold thermal conductivity(W/mK)(WF,NF)
1.600000E-05 Mold thermal expansion coeff. (1/K)
0.0000 funnel height (mm)
0.0000 funnel width (mm)
0.0000 funnel depth at mold top (mm)
3.500000 Machine outer radius(m)
3.500000 Machine inner radius(m)
6      Number of mold coating/plating thickness changes down mold
No. Scale Ni Cr Others Air gap Z-positions unit
1 0.000 0.000 0.000 0.000 0.000 (mm)
2 0.000 0.000 0.000 0.000 50.000 (mm)
3 0.000 0.000 0.000 0.000 150.000 (mm)
4 0.000 0.000 0.000 0.000 300.000 (mm)
5 0.000 0.000 0.000 0.000 500.000 (mm)
6 0.000 0.000 0.000 0.000 1100.000 (mm)
0.550 72.100 67.000 1.000 0.060 Conductivity (W/mK)
```

# Con1d9.6 input file (Cont...)

```
//MOLD THERMOCOUPLES:  
0.000000E+00 Offset distance towards hot face (mm)  
45 Total number of thermocouples  
No. Distance beneath Distance below  
hot surface(mm) meniscus(mm)  
1 0.00 -70.00  
2 0.00 -50.00  
3 0.00 -20.00  
4 0.00 -10.00  
5 10.80 0.00  
6 10.80 -20.00  
7 10.80 -50.00  
8 10.80 -20.00  
9 10.80 -10.00  
10 10.80 0.00  
11 10.80 20.00  
12 10.80 30.00  
13 10.80 50.00  
14 10.80 70.00  
15 10.80 85.00  
16 10.80 100.00  
17 10.80 120.00  
18 10.80 140.00  
19 10.80 170.00  
20 10.80 200.00  
21 10.80 250.00  
22 10.80 300.00  
23 10.80 400.00  
24 10.80 500.00  
25 10.80 600.00  
26 10.80 700.00  
27 10.80 790.00  
28 15.80 0.00  
29 15.80 20.00  
30 15.80 30.00  
31 15.80 50.00  
32 15.80 70.00  
33 15.80 85.00  
34 15.80 100.00  
35 15.80 120.00  
36 15.80 140.00  
37 15.80 170.00  
38 15.80 200.00  
39 15.80 250.00  
40 15.80 300.00  
41 15.80 400.00  
42 15.80 500.00  
43 15.80 600.00  
44 15.80 700.00  
45 15.80 790.00
```

## Future work

- Accurate Leidenfrost effect h-multipliers and temperatures needed.
- Continuous improvement for Con1d needed.